



Attitude Determination System of Small Satellite

Satellite Research Centre

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*1st Space Science School, Geo-informatics and Space Technology Development Agency
(GISTDA), Chonburi, Thailand.*



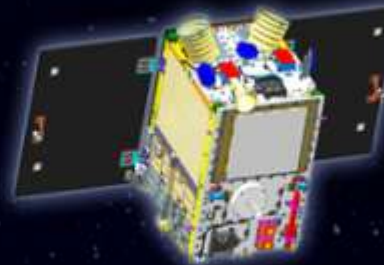
SaRC - Satellite Research Centre

To be a world class centre for advanced research and training in innovative space technologies for small satellite system

World First zigbee network in space



VELOX-I



VELOX-CI



VELOX-II



AOBA VELOX-III

Pulse plasma thruster demonstration satellite. Launch in 2016.

VELOX-PIII

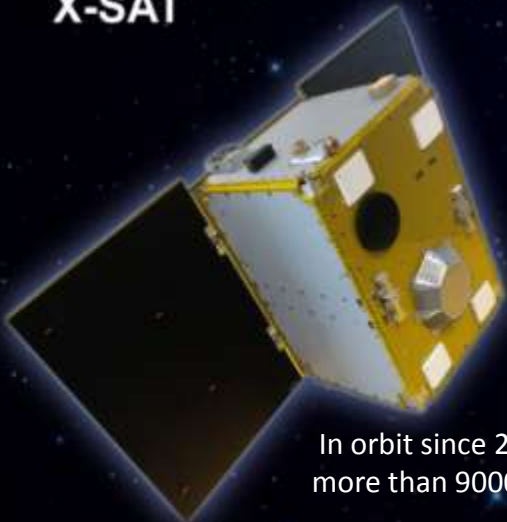


The smallest satellite with iPhone size, 193g. In orbit since 30 June 2014.

A climate research satellite using radio occultation. In orbit since 16 Dec 2015.

Inter-satellite communication demonstrating anywhere anytime up and down link. In orbit since 16 Dec 2015.

X-SAT



In orbit since 20 April 2011. It captures more than 9000 high resolution images.

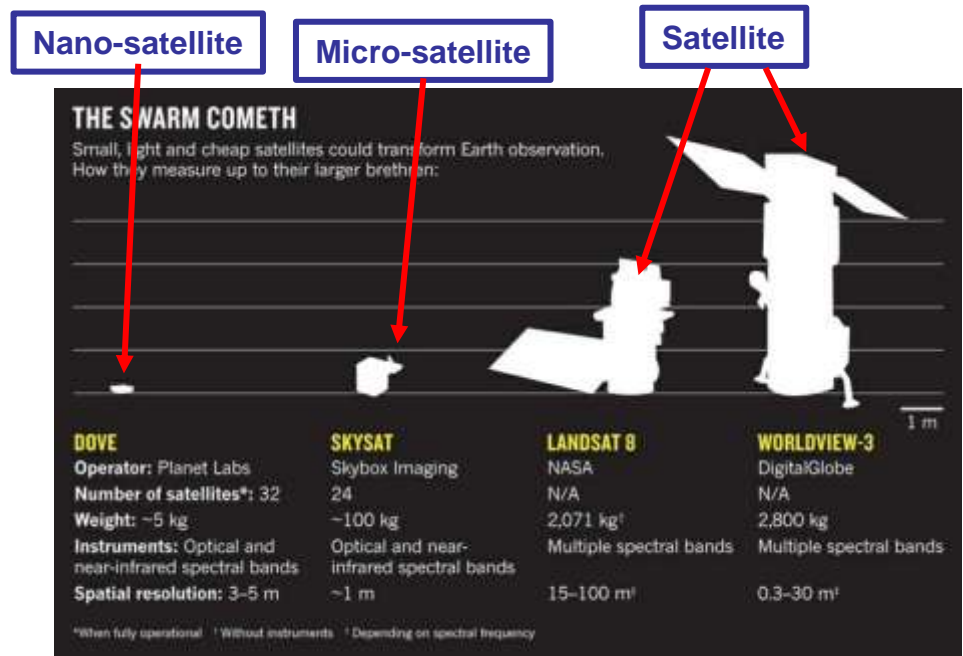
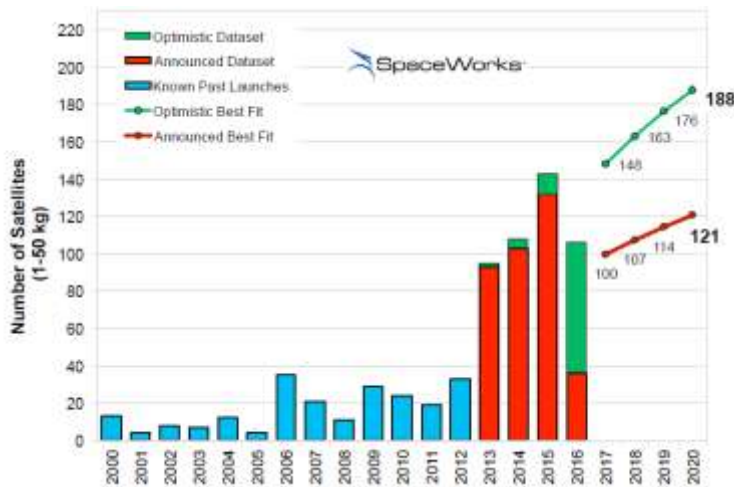
VELOX-PII



The first student built satellite. In orbit since 21 Nov 2013.

Background

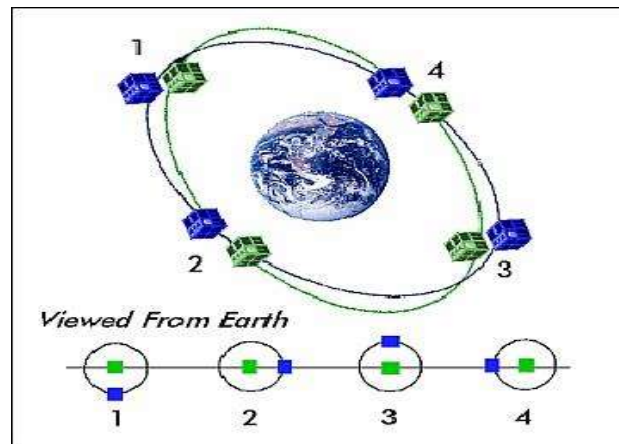
- The industry of miniature satellite has been growing. SpaceWorks' market assessment indicates around 180 nano/microsatellites requiring a launch in year 2020*.



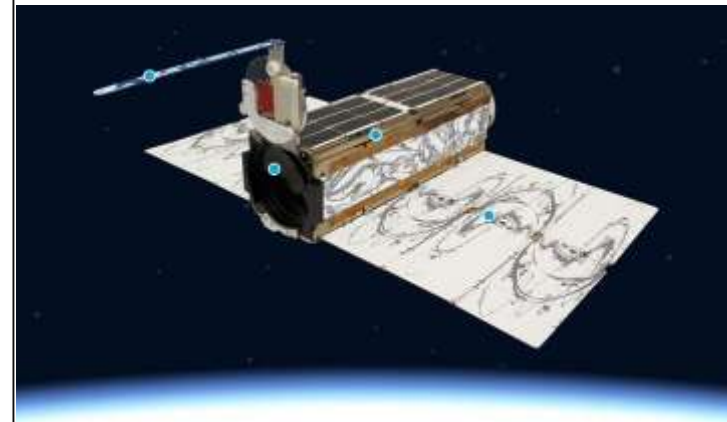
*D. DePasquale and J. Bradford, "Nano/Microsatellite Market Assessment," SpaceWorks2013.

Background

- The nano-satellites industry has changed from research purposes to application focused
 - Remote sensing
 - Automated Identification System (AIS) for ship tracking
 - Automatic dependent surveillance – broadcast (ADS-B) for aircraft position estimation
 - Intersatellite Communication
- Industry and university that constantly building nano-satellites
 - University of Toronto Institute for Aerospace Studies (UTIAS)
 - NTU Satellite Research Centre (SaRC)
 - Planet Labs
 - Spire
 - Stensat Group
 - Satellogic



Nano-satellite formation flying



DOVE by Planet Labs

Attitude determination and control system (ADCS)

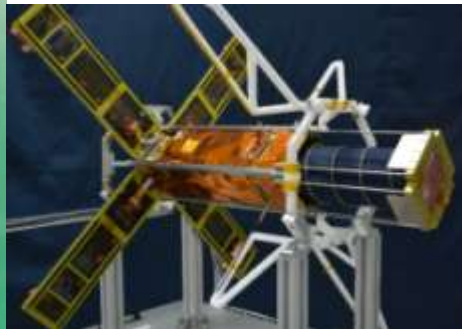
- Most applications require target tracking, precise attitude determination is important
- Nano-satellite's ADCS
 - MEMS Inertial Measurement Unit with gyroscope and magnetometer
 - Sun Sensors
 - Reaction Wheel
 - Magnetic torquer



ADCS printed circuit board



Sun sensor

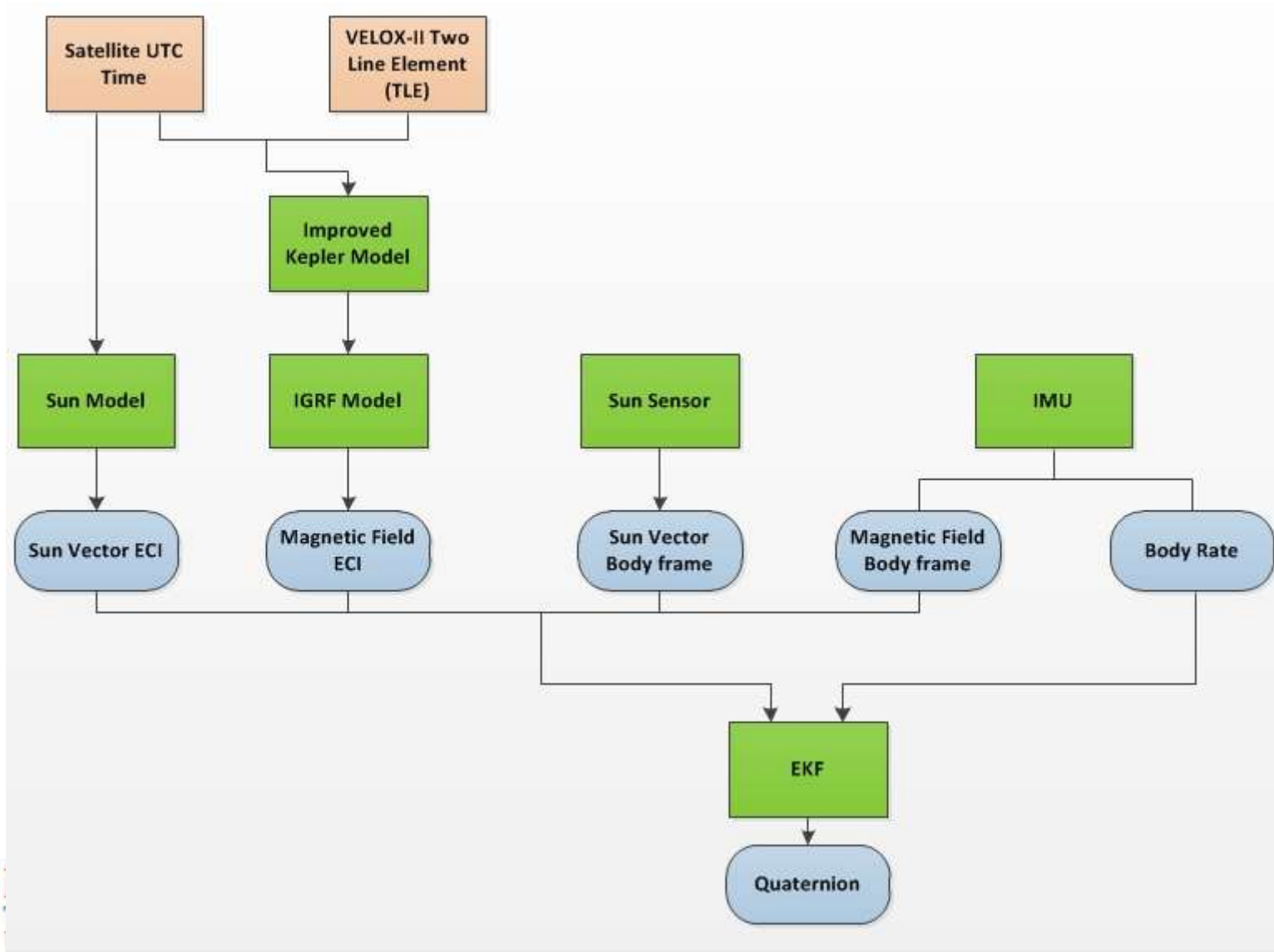


VELOX- I



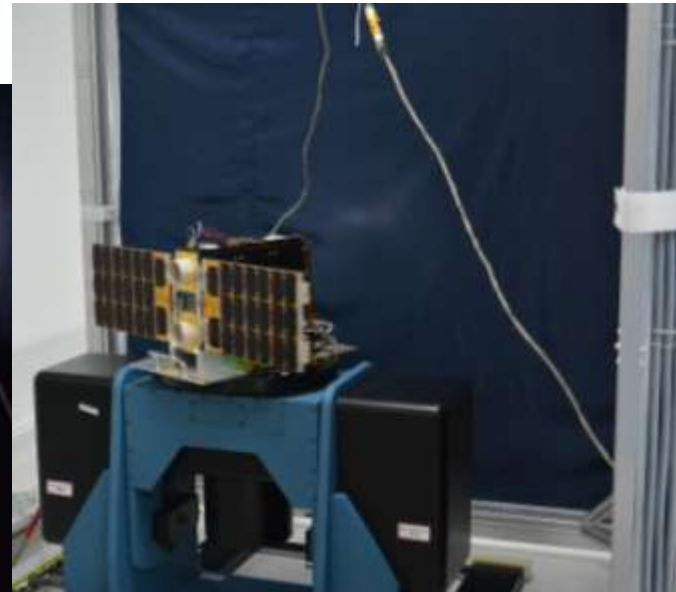
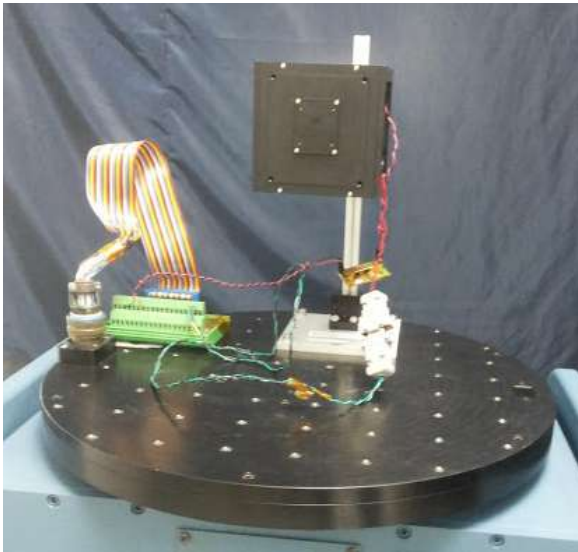
VELOX- II

Attitude Determination System (ADS)



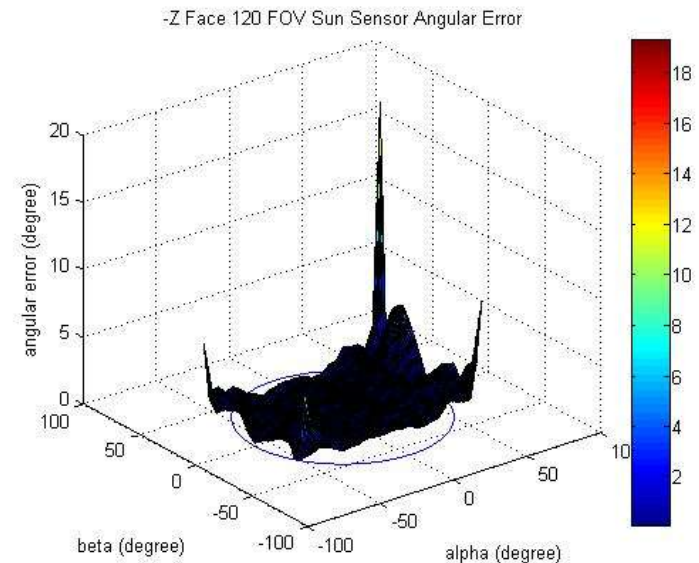
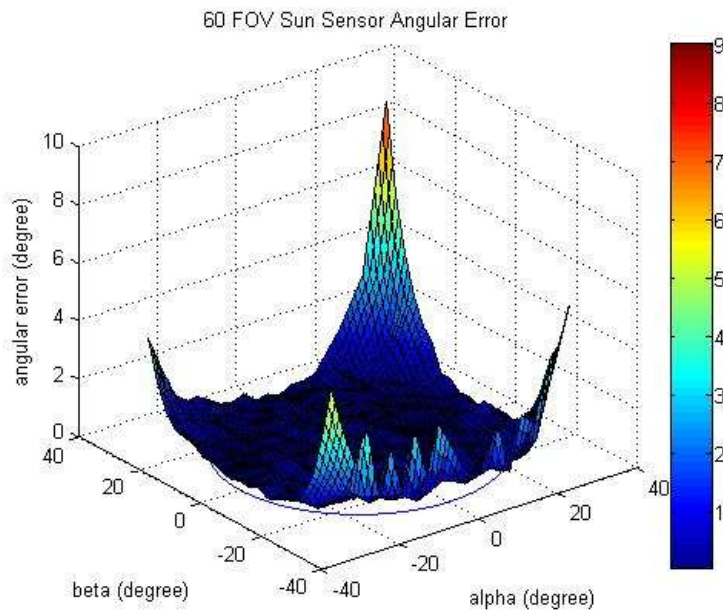
ADS: Sun Sensor

- In-house designed Analog Sun Sensor
- Consists of:
 - 2-dimensional position sensitive detector (PSD)
 - Mechanical cover



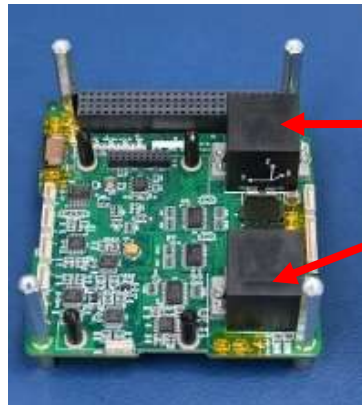
ADS: Sun Sensor

| | 60FOV | 120FOV Z- |
|----------|-------|-----------|
| RMS (°) | 0.36 | 0.82 |
| Mean (°) | 0.29 | 0.69 |
| Std (°) | 0.23 | 0.45 |

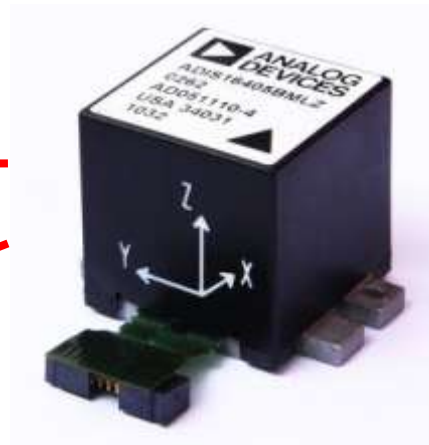


ADS: Inertial Measurement Unit

- Microelectromechanical systems (MEMS) based attitude determination system (ADS) is typically used for nano-satellites due to the limitation of
 - Size
 - Weight
 - Low computational power
- Low accuracy (noisy)



VELOX ADS
printed circuit board



Analog Devices ADIS16405
Inertial Measurement Unit (IMU)

ADS: Gyroscope

- Kalman filter to reduce the gyroscope noise
- MEMS gyroscope can be modelled as:

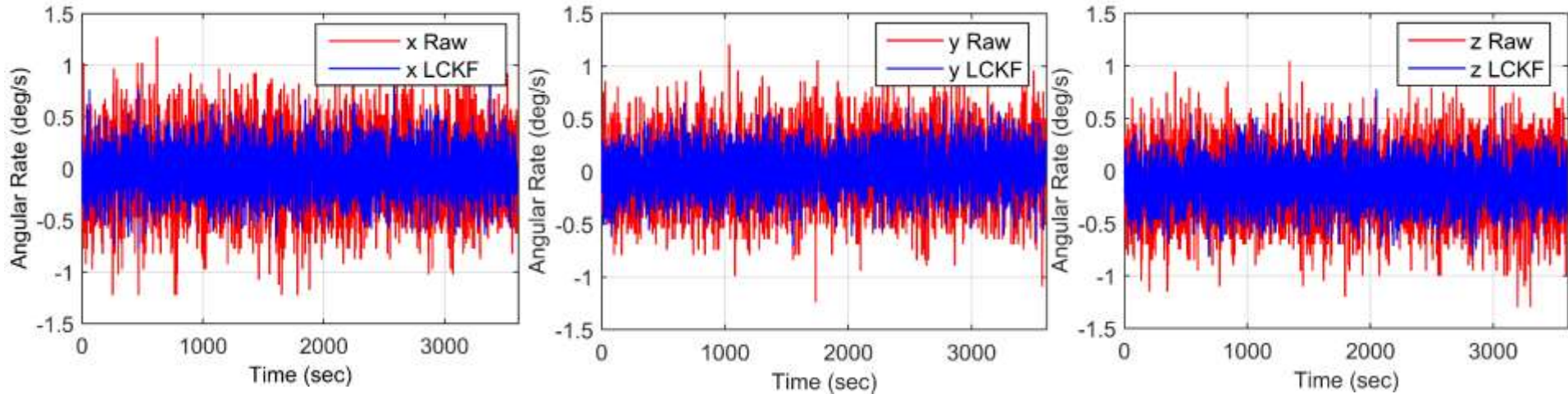
Angular rate $\xrightarrow{\quad}$ Sampling time

$$\boldsymbol{\omega}_{k+1} = \boldsymbol{\omega}_k + \dot{\boldsymbol{\omega}}_k \Delta t + \boldsymbol{\sigma}_{\text{noise}} \leftarrow \text{Gyroscope noise}$$

Angular acceleration $\xrightarrow{\quad}$

$$\dot{\boldsymbol{\omega}}_{k+1} = \dot{\boldsymbol{\omega}}_k + \dot{\boldsymbol{\sigma}}_{\text{noise}} \leftarrow \text{First order gyroscope noise}$$

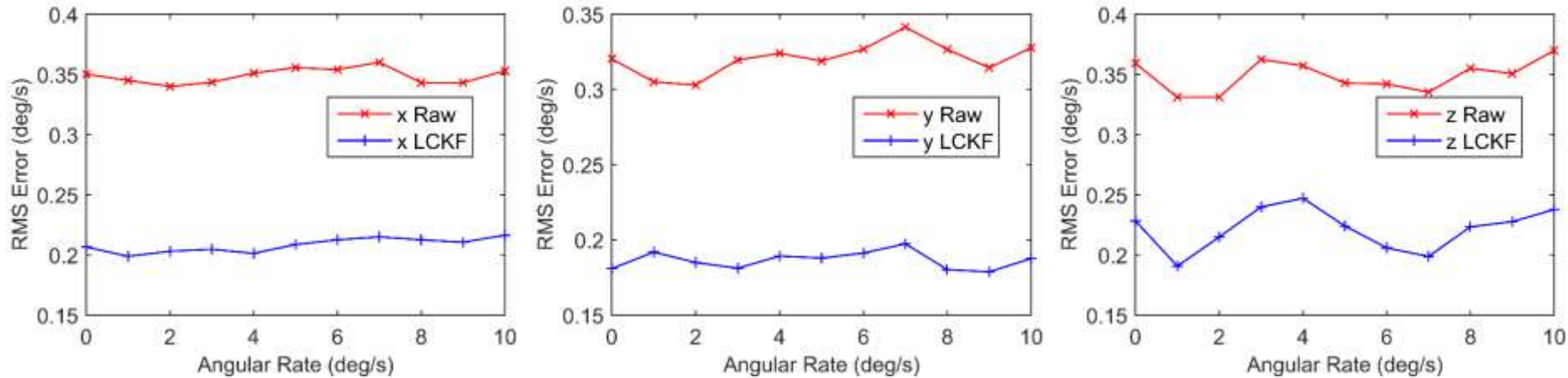
Kalman filter(KF) experimental results



Comparison of raw and KF angular rate at static condition

- Gyroscope noise reduced by 20.92%

Kalman filter(KF) experimental results



Comparison of raw and KF angular rate at dynamic condition

- **KF gyroscope angular rate in all axes has lower RMS error at any given rotation rate**

Observer free sun tracking

- VELOX sun tracking used an observer free quaternion error correction method together with Model Predictive Control.
- The general linearized control law for the observer free sun tracking algorithm is:

$$\text{Torque applied by reaction wheels} \longrightarrow \mathbf{T}_{\text{RW}} = \mathbf{G} \begin{bmatrix} \boldsymbol{\varepsilon}_e^{\text{T}} & \boldsymbol{\omega}^{\text{T}} \end{bmatrix}^{\text{T}}$$

Control Gain matrix \longleftarrow

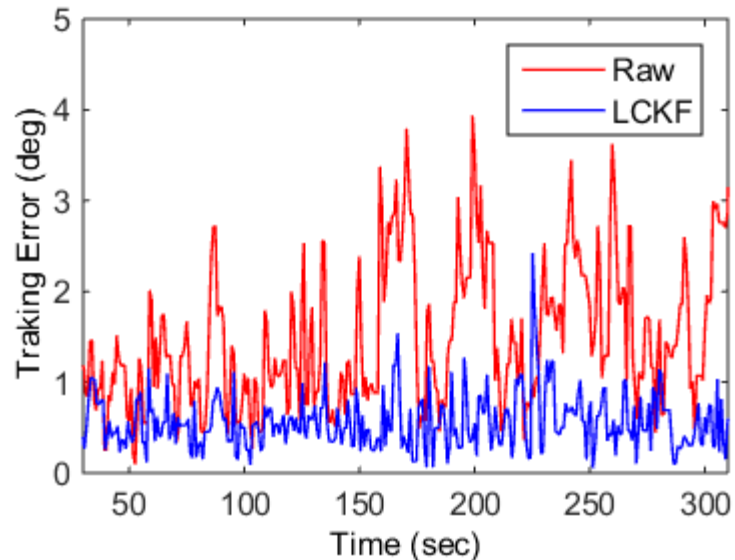
Satellite body rate \longleftarrow

Vector component of error quaternion \longleftarrow

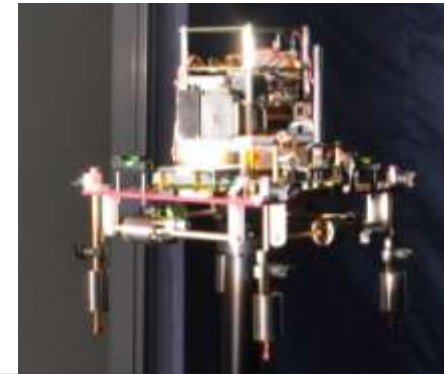
- Highly susceptible to gyroscope noise

Observer free sun tracking: experiment

- RMS steady state tracking error without KF is 1.672° whereas with KF is 0.622°



Sun tracking error at steady state

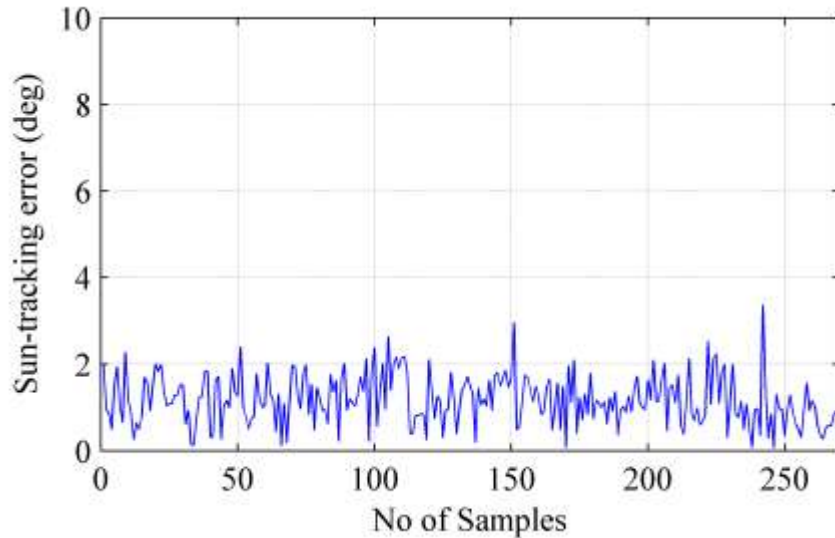


Spacecraft simulator

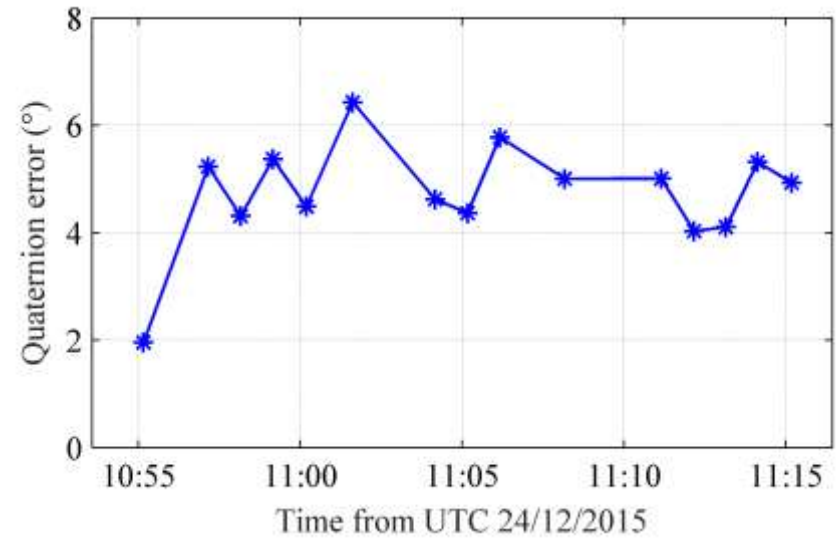


Sun tracking experimental setup

VELOX-II ADCS In-orbit result



Sun tracking performance of VELOX-II on 1st Feb 2016



Performance of nadir pointing conducted on 24th Dec 2015

Future Work

- **Digital sun sensor development**
 - Complementary metal-oxide-semiconductor (CMOS)
- **In-orbit gyroscope and magnetometer calibration**
 - Thermal variation
 - On-board electronics time-varying bias
 - Mechanical mis-alignment
 - Gyro bias drift (gyroscope)
 - Coupling effect of magnetic torquer (magnetometer)



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